

impedance iaround 5 k . Sinking too much of current from						

Although differential input rejects commommode noise inherently, the common mode voltage on each of the input pin still affects the operation of the controller. A common mode filter is generally implemented to filter out the common mode noise. Figure 11. shows a schematic of the common mode filter. Bandwidth of the common mode filteris

$$f_{BW-comon} = \frac{1}{2 \cdot R_f \cdot C_C}$$
 (eq. 7)

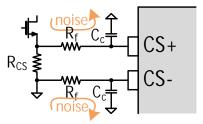


Figure 11. Common imode Filter for CS Pin

A resistance value connecting between VIR and GND decides the voltage on the VIR pin. The voltage on the VIR pin needs to be set higher than 3.5 V or lower than 1.5 V. Avoid anything in between.

The setting on the VIR pin changes some internal signals of FAN967x, which are collected in Table 1. M_{RLPK} constant appears in the ble. According to the test cases of V_{LPK} , which can be found in electrical characteristics in the datasheet, M_{LPK} is 2.465.

Table 1. Effects of VIR Setting

V_{VIR}	< 1.5 V	> 3.5 V
Optimized for	Universal ïinput range (90~264 Vac)	European iinput

Due to a mismatch between the resistors and capacitors in the common mode filter, common mode noise may be filtered differently between CS+ and CSAs a result, a differential mode noise appears the CS signals. To tackle with the differential mode noise, we add a capacitor to filter out the differential mode noise.

With the resultant CS filter in Figure 12, which combines commonimode and differential imode filters, the bandwidth of a lowpass filter for the differential CS signals becomes

$$f_{\text{BW-diff}} = \frac{1}{2 \cdot 2R_f \cdot C_d + \frac{1}{2} \cdot C_c}$$
 (eq. 8)

The bandwidth of the filter should be set based on noise that isgenerated in actual design restricts 5 kW reference design for FAN9673 with 40 kHz of switching frequency, we set FBW common at 154 kHz and FBW diff at 51.3 kHz.

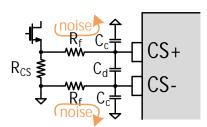


Figure 12. CS Pin Filter

Effect of Input Range Setting

VIR pin of FAN967x sets two different modes that optimize for universal input range and European input range, respectively. This pin sources a constant current.

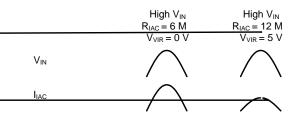


Figure 16. V $_{\rm IN}$ Related Signals under Different VIR and R $_{\rm IAC}$ Setting

To make inductor track current command well, the bandwidth of the current tracking loop need to set high enough. When the complex pole formed Lby ndC_{OUT} is at a frequency much lower than the control bandwidth of $T_I(s)$

$$\text{Loopgain(s)} \quad \frac{(V_{\text{IN.PEAK}} \mid \text{sin(t)} \mid)^2}{V_{\text{IN.RMS}}^2} \quad \frac{1}{V_{\text{OUT}}} \quad \frac{1}{s} \quad \frac{1}{C_{\text{OUT}}} \quad \frac{P_{\text{MAX}}}{(V_{\text{VEA.MAX}} \quad 0.6)} \quad \frac{V_{\text{FBPFC}}}{V_{\text{OUT}}} \quad G_{\text{mv}}(s)$$
 (eq. 25)
$$\text{Loopgain(s)}_{\text{ac} \quad \text{cycle}} \quad \frac{1}{s} \quad \frac{P_{\text{MAX}}}{C_{\text{OUT}}} \quad (V_{\text{VEA.MAX}} \quad 0.6) \quad V_{\text{OUT}}$$